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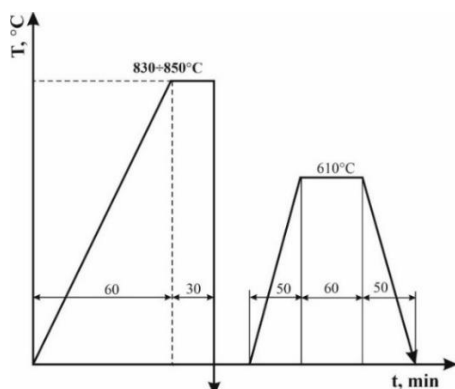


Fig.2. Time-temperature curve of the thermal treatment of the parts.

TABLE 1 CHEMICAL COMPOSITION OF THE STEEL

C	Si	Mn	Ni	Cr	Mo	P	Cu
0.405	0.239	0.652	0.110	0.894	0.180	0.012	0.227

The experiments were conducted in industrial conditions on a HARRIS C320KTT CNC lathe – Fig. 3, with an RV-8CRL robotic feeding station – Fig. 4.



Fig. 3. General view of the HARRIS C 320KTT CNC lathe.



Fig.4. Robotic station RV-8CRL.

The roughness of the machined surfaces was measured on the inner diameters of the parts Ø50.85 and Ø46.85 with a TESA Rugosurf 20 profilometer using the criterion "arithmetic mean deviation from the profile centerline" - Ra.

III. RESULTS AND DISCUSSION

In order to analyze the machinability of the details in the robotic feeding, mathematical models were compiled and a statistical analysis was conducted – Anova (Analysis of Variance). In it, the cutting speed (V_c , m/min) – X_1 , and the feed (f , mm/rev) – X_2 , were selected as input variables (controlled factors). The average roughness (R_a , μm) of the machined internal surfaces – Y_1 (Ø50.85) and Y_2 (Ø 46.85) were studied as objective functions.

The compilation of the mathematical models is based on the obtained experimental results at cutting speed - V_c 140÷180 mm/min and feed - f 0.045÷0.065 mm/tur.

Table 2 presents the levels of variation of the controlling factors, and Table 3 presents the average values of the studied parameters used to compile the mathematical model.

Based on the values in Table 3, the experimental plan was completed – Table 4.

TABLE 2 LEVEL OF VARIATION

Areas of variation	X_1 , (V_c , m/min)	X_2 , (f , mm/tur)	Coded values
$X_{i0} + \Delta X_i$	180	0,65	+1
X_{i0}	160	0,55	0
$X_{i0} - \Delta X_i$	140	0,45	-1

TABLE 3 AVERAGE EXPERIMENTAL RESULTS

X_1 , (V_c , m/min)	изследвани параметри	X_2 , (f , mm/tur)		
		0,45	0,55	0,65
140	Y_1 , (Ra, μm)	0,248	0,346	0,445
	Y_2 , (Ra, μm)	0,268	0,359	0,470
160	Y_1 , (Ra, μm)	0,186	0,244	0,311
	Y_2 , (Ra, μm)	0,248	0,291	0,347
180	Y_1 , (Ra, μm)	0,158	0,188	0,240
	Y_2 , (Ra, μm)	0,208	0,602	0,309

TABLE 4 EXPERIMENTAL PLAN

Nº	X_0	X_1	X_2	$X_1 X_2$	X_1^2	X_2^2	Y_1 (Ra, μm)	Y_2 (Ra, μm)
1	+1	+1	+1	+1	+1	+1	0,240	0,309
2	+1	-1	+1	-1	+1	+1	0,445	0,470
3	+1	+1	-1	-1	+1	+1	0,158	0,208
4	+1	-1	-1	+1	+1	+1	0,248	0,268
5	+1	+1	0	0	+1	0	0,188	0,602
6	+1	-1	0	0	+1	0	0,346	0,359
7	+1	0	+1	0	0	+1	0,311	0,347
8	+1	0	-1	0	0	+1	0,186	0,248
9	+1	0	0	0	0	0	0,244	0,291

The processing of the obtained results for the studied objective functions – Y_1 and Y_2 , leads to the determination of linear regression equations of the type:

$$Y_{1,2} = b_0 - b_1 x_1 + b_2 x_2 - b_{11} x_{11} + b_{22} x_{22} - b_{12} x_{12} \quad (1)$$

The calculated model coefficients for Y_1 and Y_2 according to [26] – [34] are presented in Table 5.

TABLE 5 COEFFICIENTS OF REGRESSION EQUATIONS

	b_0	b_1	b_2	b_{11}	b_{22}	b_{12}
Y_1	0,2423	-0,0772	0,069	-0,0255	0,007	-0,0313
Y_2	1,2032	-0,3068	0,2217	-0,0448	0,0057	-0,041

The obtained regression models for determining the average roughness Y_1 and Y_2 (R_a , μm) are represented by equations 3 and 4.

$$Y_1 = 0,2423 - 0,0772X_1 + 0,069X_2 - 0,0255X_{11} + 0,007X_{22} - 0,0313X_{12} \quad (3)$$

$$Y_2 = 1,203 - 0,3068X_1 + 0,2217X_2 - 0,0448X_{11} + 0,0057X_{22} - 0,041X_{12} \quad (4)$$

The adequacy check of the models according to the Fisher criterion [35] – [37] shows that they are adequate.

The graphical dependencies for 3 and 4 are presented in Fig. 4 and 6, respectively.

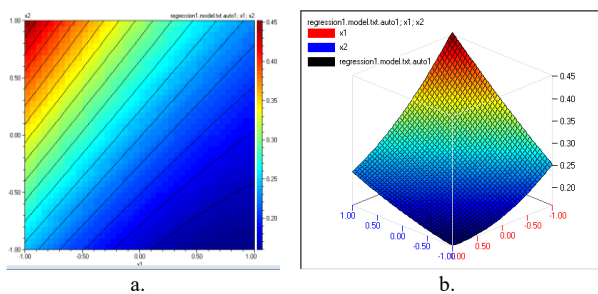


Fig.3. Visualization of the solutions of the regression model for $Y_1(R_a, \mu m)$ when machining a hole $\varnothing 50.85$ in two- and three-coordinate systems (a and b).

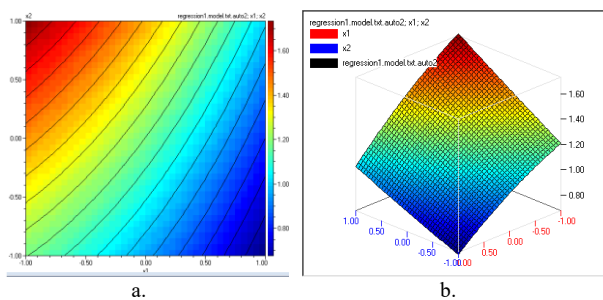


Fig.4. Visualization of the solutions of the regression model for $Y_1(R_a, \mu m)$ when machining a hole $\varnothing 46.85$ in two- and three-coordinate systems (a and b).

When conducting the analysis of variance of the model, Qv Stat Lab Anova was used. The graphical interpretation of the results for the three coded values for Y_1 and Y_2 (R_a , μm) are presented in Fig. 5 and 6, respectively.

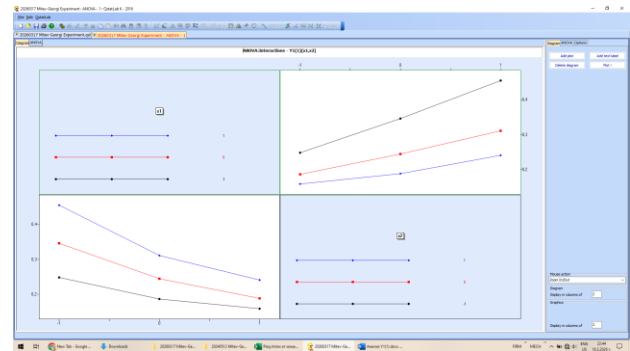


Fig. 5. Analysis of variance of the dependence $Y_1 = f(X_1, X_2)$ at X_{-1} ; X_0 and X_{+1} .

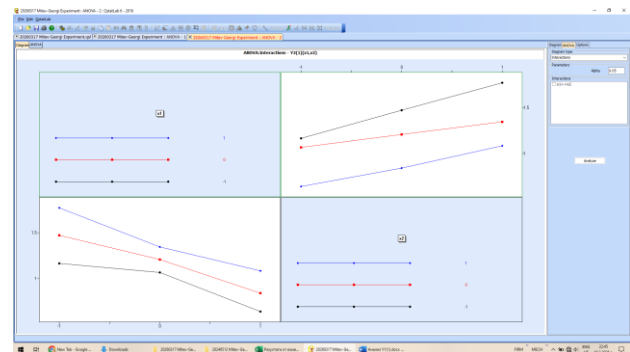


Fig. 6. Analysis of variance of the dependence $Y_2 = f(X_1, X_2)$ at X_{-1} ; X_0 and X_{+1} .

The optimization of the technological process for the machinability of short rotary parts from improveable steels with robotic feeding was made based on set values Y_1 min and Y_2 min. It was carried out by random search with increasing density (genetic algorithm) [31] – [33]. The graphical interpretation is shown in Fig. 7 and 8. for machined holes $\varnothing 50.85$ and $\varnothing 46.85$, respectively.

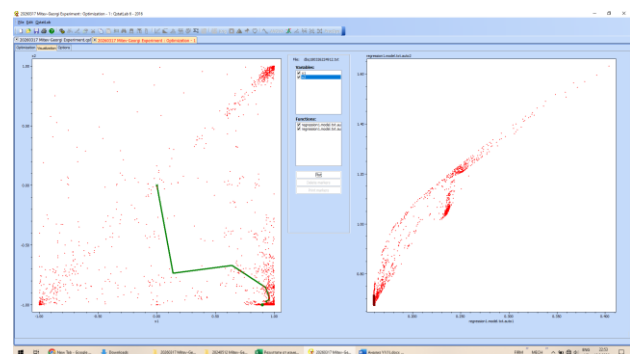


Fig.7. Optimization of the technological process for machining holes $\varnothing 50.85$ at Y_1 min.

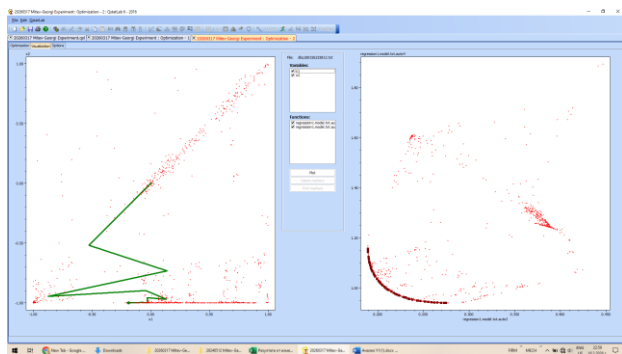


Fig.7. Optimization of the technological process for machining holes Ø46.85 at Y₂min.

IV. CONCLUSIONS

The following more important conclusions can be formulated from the conducted research and the results obtained:

- The machinability of improved medium-alloy structural steels was studied when machining short rotary parts on CNC lathes with robotic feeding according to the criterion of average roughness deviation on the machined surfaces - Ra.
- Empirical models of the studied functions were compiled and their adequacy was checked using the Fisher criterion.
- The dispersion analysis performed has shown that optimal working conditions for the given material, speed and feed are achieved at $V_c = 180$ m/min and $f = 0.45$ mm/tur.
- The optimization of the technological process was done based on the given values Y₁ min and Y₂ min. It was carried out by random search with increasing density (genetic algorithm).

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