

Influence of Strength Characteristics on the Technological Parameters of the Boroaluminizing Process

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Abstract— At present, data on the influence of boroaluminizing on the mechanical properties of steels are scarce and contradictory. This publication presents a mathematical model for determining the strength characteristics of medium-alloyed quality steel and their influence on the technological characteristics of the boroaluminizing process (saturation times, quenching and tempering temperatures). Based on the mathematical model, graphical relationships for R_m , $R_{0.2}$ and A_5 as a function of the technological characteristics of the boroaluminizing process have been developed.

Keywords— boroaluminizing, diffusion, proportional limit, relative elongation, tensile strength.

I. INTRODUCTION

The development of modern mechanical engineering and other branches of industry in the context of Industry 4.0 is inextricably linked to placing high demands on the properties of parts and tools [1, 2, 3, 4, 5, 6, 7, 8, 9, 10].

There are increasingly frequent cases when structural and tool materials must have high hardness, strength and resistance in oxidizing and highly aggressive environments. All this can be achieved with the methods of chemical-thermal treatment. In this technological process, diffusion layers with fundamentally new phases are created on the surface, fully satisfying the set requirements. Moreover, the formed diffusion layer, as a result of reducing defects in the structure of the part, brings its working surface closer to the ideal, which increases the durability of the product as a whole [11, 12].

The choice of saturating elements is determined by the desired complex of mechanical properties of the particular part, but in any case it is necessary that the formation of the diffusion layer is accompanied by a decrease in the thermodynamic potential of the surface and an increase in the forces of interaction of atoms. Moreover, the greater the

change in the specified characteristics, the higher the physicochemical and mechanical properties of the layer.

Currently, processes related to single-component saturation of parts – carburizing, nitriding, boriding, etc. [13, 14, 15, 16, 17, 18, 19] Saturation with two, three or more elements (with the exception of the nitrocarburizing process) are widely used in practice.

The possibility of simultaneous saturation with boron and aluminum was established in the eighties of the last century [20, 21, 22, 23, 24]. The first results show an exceptional perspective of the obtained diffusion layers for protecting the parts from abrasive impact. Subsequently, it was proven that the properties of the boron-alloyed layers depend on the ratio of diffusing boron and aluminum atoms in the surface of the part, but in all cases they have:

- high microhardness $14 \div 19000$ MPa, and when saturated with high-alloy steels up to 21000 MPa;
- high abrasion resistance exceeding that of heat-treated steels by $3 \div 18$ times;
- resistance to heating in an oxidizing environment up to 950°C ;
- resistance in sulfur-containing and other active gas environments.

However, this method has not found wide application due to insufficient knowledge of the technological processes occurring during saturation [25, 26, 27, 28, 29].

In this regard, the purpose of this publication is to trace the influence of the technological processes of boroaluminum on the main strength characteristics of diffusion-enriched samples of medium-alloyed high-quality structural steels [30, 31].

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II. MATERIALS AND METHODS

The study used samples of medium-alloyed high-quality structural steel 34CrNiMo6 EN ISO 6892-1:2020, with chemical composition according to Table 1 and mechanical properties in the as-delivered condition $R_m=1100\text{MPa}$, $R_{0.2} 900\div 1000\text{MPa}$ and HB 229.

TABLE 1 CHEMICAL COMPOSITION

Chemical composition, %							
	C	Cr	Mn	Si	P	S	Fe
min	0,32	0,80	0,80	1,10	$\leq 0,025$	$\leq 0,025$	$> 96,00$
max	0,38	1,10	1,10	1,40			

The diffusion enrichment of the samples was carried out in a liquid saturating medium. Borax ($\text{Na}_2\text{B}_4\text{O}_7 \cdot 10\text{H}_2\text{O}$), boric anhydride (B_2O_3) and alumina (Al_2O_3) were used as carriers of active atoms in the diffusion medium, and boron carbide (B_4C) was used as a reducing agent.

The saturation temperature is $820\div 880^\circ\text{C}$, and the duration is $120\div 240$ min. After saturation, the samples are quenched (from the saturation temperature) in an oil bath and subjected to high-temperature annealing at $500\div 600^\circ\text{C}$.

The annealing duration of the standard test specimens for tensile strength testing is constant - 1 h.

The strength characteristics test according to EN 1002 was conducted on an automatic hydraulic, universal tensile/compression testing machine with an optical control module with a touch screen display, maximum tensile force 700kN and accuracy of results $\pm 1\%$ - Fig. 1.



Fig.1. Universal tensile strength testing machine

III. RESULTS AND DISCUSSION

The mechanism of influence of boroaluminizing diffusion coatings on the mechanical properties of the studied samples after saturation and subsequent heat treatment was investigated using mathematical planning of the experiment using a second-degree orthogonal

compositional design [40]. On this basis, adequate regression equations modeling the saturation regime and the subsequent heat treatment were derived.

The tensile strength – Y_1 (R_m , MPa), the proportionality limit – Y_2 ($R_{0.2}$, MPa), and the conditional relative elongation at break – Y_3 (A_5 , %) were used as control functions.

The input factors (parameters) are the saturation temperature – X_1 (T_1 , $^\circ\text{C}$), from which the parts are immediately quenched in oil, the saturation duration – X_2 (t , min), and the tempering temperature – X_3 (T_2 , $^\circ\text{C}$).

The main levels of input factors, as well as the variation intervals, are presented in Table 2.

TABLE 2 INPUT FACTORS

	Input factors		
	X_1 , T_1 , $^\circ\text{C}$	X_2 , t , min	X_3 , T_2 , $^\circ\text{C}$
Basic level	850	180	550
Variation interval	30	60	50
Upper level	880	240	600
Lower level	820	120	500

When implementing the experimental plan, analytical dependencies were established for the control functions on the specified factors 1÷3.

$$Y_1 = 13220 - 35X_1 + 8,4X_2 + 10,8X_3 + 0,025X_1^2 + 0,0076X_2^2 - 0,0021X_3^2 - 0,0073X_1X_2 - 0,0124X_1X_3 - 0,068X_2X_3 \quad (1)$$

$$Y_2 = 15816 - 38,9X_1 - 0,7X_2 + 8,58X_3 + 0,025X_1^2 + 0,013X_2^2 - 0,0032X_3^2 - 0,0027X_1X_2 - 0,086X_1X_3 - 0,0029X_2X_3 \quad (2)$$

$$Y_3 = 28,6 + 0,044X_1 + 0,017X_2 + 0,02X_3 - 0,00008X_1^2 - 0,00009X_2^2 - 0,000009X_3^2 - 0,000012X_1X_2 - 0,00001X_1X_3 - 0,0002X_2X_3 \quad (3)$$

The graphical interpretations of the obtained dependencies are presented in Fig. 1÷3.

Through them, with given values for R_m , $R_{0.2}$ and A_5 , the optimal values of the technological parameters of diffusion saturation (temperature and duration of saturation) with boron and aluminium can be determined.

The graphical dependences show a stronger influence of the tempering temperature on the studied mechanical characteristics than the saturation temperature and duration. This indicates that the strengthening during simultaneous diffusion of boron and aluminium into the surface of the samples is a result of an increase in the amount of pinned dislocations on the surface of the strengthened samples [32, 33, 34, 35].

Boron is known to be a surface active element with respect to iron. The absorption of boron along dislocation lines creates an atmosphere analogous to that of Cottrell of carbon atoms. This allows for easier pinning of dislocations

and lowers the linear stresses around them. At the same time, their density increases. The latter is stimulated by the effects of stresses arising from the diffusion of boron and aluminium [36, 37, 38, 39].

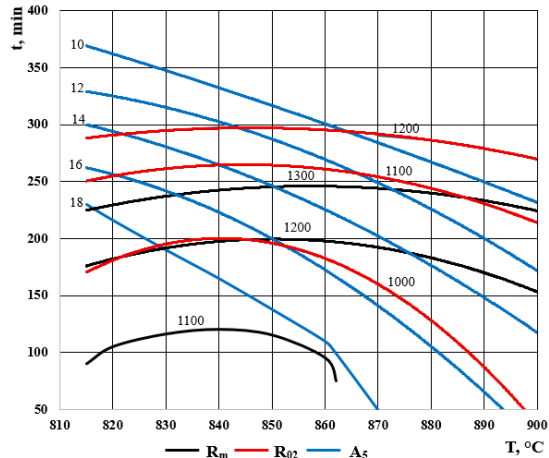


Fig. 1. Dependences of the strength characteristics of boroaluminizing samples on the technological parameters of the process at a tempering temperature of 500°C.

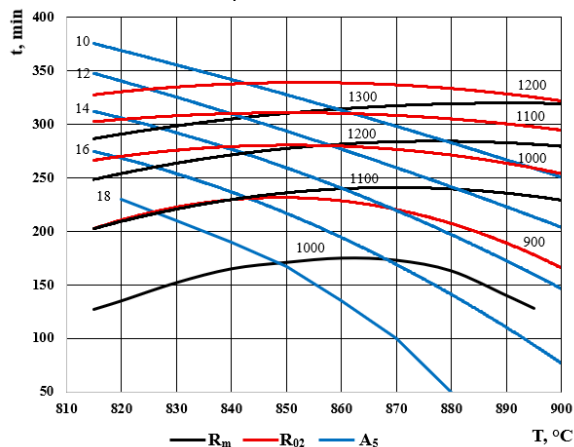


Fig. 2. Dependences of the strength characteristics of boroaluminizing samples on the technological parameters of the process at a tempering temperature of 550°C.

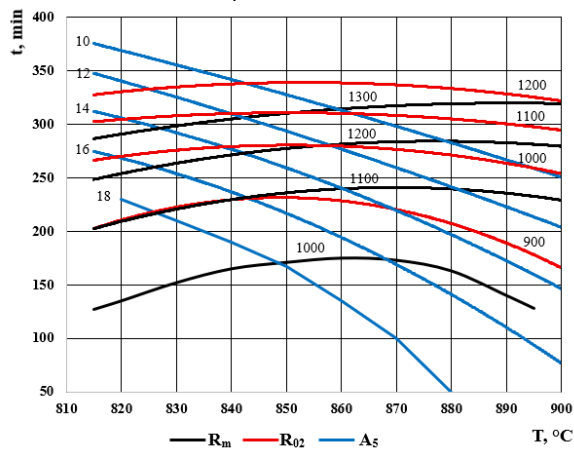


Fig. 3. Dependences of the strength characteristics of boroaluminizing samples on the technological parameters of the process at a tempering temperature of 600°C.

Furthermore, the formation of the borides FeB and Fe₂B with elastic moduli of 350 and 290.10³ MPa, respectively, significantly exceeding the elastic modulus of steel, increases the elastic modulus on the surface of the product. This increases the resistance to the movement of dislocations and their emergence to the surface.

Therefore, the strength characteristics of steels after simultaneous diffusion enrichment with boron and aluminum are determined by the structural state of the formed diffusion layer and to a lesser extent by its thickness. The diffusion of boron and aluminium and the formation of borides on the surface of the parts change the density and energy of the dislocations (the structural energy state of the saturated surface), which leads to a change in the bulk properties of the product as a whole [40].

IV. CONCLUSIONS

From the conducted studies and the results obtained, the following important conclusions can be formulated:

- The mechanism of influence of boroaluminizing diffusion coatings on the strength properties of 34CrNiMo6 steel after saturation in liquid media at 820÷880 °C, with a duration of 120÷240 min and subsequent heat treatment (quenching from the saturation temperature and high-temperature tempering) was studied.
- Mathematical models of the process were constructed using a second-degree orthogonal compositional design and adequate regression equations were derived.
- Graphical relationships have been developed to determine the technological parameters of the boroaluminizing process (temperature and duration) depending on the desired strength properties (R_a, R_{0.2} and A₅) of the product.
- It has been proven that the influence of the tempering temperature on the studied mechanical characteristics is stronger than the temperature and duration of saturation.

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